

ANALYTICAL REPRESENTATION OF THE RESULTS  
OF A NUMERICAL DETERMINATION OF THE  
THERMODYNAMIC CHARACTERISTICS OF  
COMBUSTION PRODUCTS

I. I. Polyakov

UDC 621.454

Approximate formulas are given for determining the ideal values of the specific impulses in a vacuum, the characteristic velocity, and the geometric expansion ratio of a supersonic nozzle.

Fuels whose combustion products are high-temperature, multicomponent, chemically reacting mixtures have found application in present-day heat technology. Results are published in the handbook [1] on the numerical integration of the problem of determining the ideal values of the thermodynamic characteristics of fuel combustion products, based on oxygen, fluorine, and other oxidants and fuels containing hydrogen, carbon, light metals, and other chemical elements. In the practical application of these data, it is necessary to resort to the interpolation of functions of two arguments - the stagnation flow pressure and the expansion ratio of the gas in the nozzle.

For the purpose of facilitating the problem of determining the optimum parameters of engines operating on the above-mentioned fuels, approximate analytical relations which describe the results of a numerical determination of the ideal values of the specific impulses in a vacuum, the characteristic velocity, and the geometric expansion ratio of the nozzle are obtained in the present paper. By specific impulse, we understand the ratio of the engine thrust to the mass fuel consumption; by the characteristic velocity we understand the product of the stagnation flow pressure and the area of the minimum cross section of the nozzle, referred to the mass fuel consumption; and by the geometric expansion ratio of the nozzle we understand the ratio of the area of the outlet section of the nozzle to the area of its minimum cross section.

The following quantities will be taken as the defining dimensionless criteria: the expansion ratio of the gas in the nozzle  $\varepsilon$ , equal to the ratio of the stagnation flow pressure to the static pressure in the outlet section of the nozzle; the relative pressure  $\pi$ , equal to the ratio of the stagnation flow pressure to the normal pressure  $p_n = 101,325 \text{ N/m}^2$ .

For  $\varepsilon = 50-5000$  and  $\pi = 5-500$ , the results of the calculations given in the handbook [1] can be described by the following empirical relations:

specific impulse in a vacuum,

$$I = I_0 [1 + a_1 \pi^{-0.5} + (a_2 + a_3 \pi^{-0.25}) f]^{-1},$$

where

$$f = \varepsilon^{-0.25} + a_4 \varepsilon^{-0.75} - \varepsilon^{-1.25};$$

characteristic velocity,

$$\beta = \beta_0 [1 - b_1 \exp(-\omega_1 \pi^{0.125}) + b_2 \exp(-\omega_2 \pi^{0.5})];$$

geometric expansion ratio of the nozzle,

$$F = c_1 + (c_2 + c_3 \pi^{-6}) \varepsilon^n,$$

Translated from *Inzhenerno-Fizicheskii Zhurnal*, Vol. 31, No. 5, pp. 844-846, November, 1976. Original article submitted October 7, 1975.

This material is protected by copyright registered in the name of Plenum Publishing Corporation, 227 West 17th Street, New York, N.Y. 10011. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, microfilming, recording or otherwise, without written permission of the publisher. A copy of this article is available from the publisher for \$7.50.

TABLE 1. Approximation Coefficients for an Oxygen-Hydrogen Fuel

Designation and dimension	Excess oxidant coefficient			
	0,4	0,6	0,8	1,0
$I_0$ , m/sec	4756	4975	5091	5161
$a_1$	0	0	-0,015	0,020
$a_2$	0,402	0,512	0,626	0,805
$a_3$	0,002	0,046	0,179	0,220
$a_4$	1,83	1,36	0,89	0,67
$\beta_0$ , m/sec	2439	2404	2359	2250
$b_1$	0,107	0,316	0,259	0,278
$w_1$	4,0	2,2	1,2	1,1
$c_1$	0,2	0,1	0	-0,1
$c_2$	0,375	0,369	0,328	0,378
$c_3$	0	0,040	0,113	-0,062
$c_4$	0	0,250	0,125	0,500
$c_5$	0,710	0,736	0,760	0,778
$c_6$	0	0	0	0,056

where

$$n = c_5 + c_6 \pi^{-0,25}.$$

Here  $I_0$  is the specific impulse in a vacuum as  $\epsilon$  and  $\pi \rightarrow \infty$ , and  $\beta_0$  is the characteristic velocity as  $\pi \rightarrow \infty$  for the assumed mathematical model of the problem. The other coefficients in these formulas are dimensionless quantities.

The numerical values of the quantities  $I_0$  and  $\beta_0$  and all the dimensionless coefficients occurring in the proposed relations have been determined for each specific fuel composition from the results of the numerical values of  $I$ ,  $\beta$ , and  $F$  for a number of values of the defining criteria. As an example, Table 1 shows the results of a determination of these coefficients for the combustion products of a liquid oxygen-liquid hydrogen fuel. In the example considered, the quantities  $b_2$  and  $w_2$  are equal to zero.

The proposed relations have been verified according to the data published in [1] and show that in the range of variation of the criteria  $\epsilon$  and  $\pi$  considered, the error in determining the quantities  $I$  and  $\beta$  does not exceed 0.1% and for the quantity  $F$ , 1%.

#### NOTATION

$I$  is the specific impulse in a vacuum;  
 $\beta$  is the characteristic velocity;  
 $F$  is the geometric expansion ratio;  
 $\epsilon$  is the expansion ratio of gas in nozzle;  
 $\pi$  is the relative pressure;  
 $p_n$  is the normal pressure;  
 $a, b,$   
 $c,$  and  $w$  are the dimensionless coefficients.

#### LITERATURE CITED

1. V. E. Alemasov et al., Thermodynamic and Thermophysical Properties of Combustion Products [in Russian], Vols. 1-7, Izd. VINITI, Akad. Nauk SSSR (1971-1974).